

Activated Sludge Math

1. Find the surface overflow rate for a secondary clarifier that is 120 feet in diameter when the influent flow is 120 gpm. Then, find the weir loading rate.
2. The liquid train for a 4.0 MGD WWTP consists of screening, grit removal, primary clarification, activated sludge, secondary clarifiers, and chlorine disinfection. The influent contains 350 mg/L of BOD. If the primary clarifiers removed 35% of the influent BOD, what is the organic load to the secondary treatment process?
3. Calculate the Sludge Volume Index (SVI) for two different operating conditions. In situation one, the MLSS concentration is 3,000 mg/L and the settled sludge volume after 30 minutes (SSV_{30}) is 250 mL. In situation two, the MLSS concentration is 8,000 mg/L and the SSV_{30} is 980 mL.
4. A treatment plant has one aeration basin and one clarifier. The aeration basin holds 300,000 gallons and the clarifier holds 60,000 gallons. The MLSS concentration is 2500 mg/L, the RAS and WAS concentrations are 7,000 mg/L, and the clarifier core concentration is 600 mg/L. Find the SRT if the WAS pump operates continuously at 10 gpm.
5. A treatment plant does not have flow monitoring on their Return Activated Sludge line. The operator wants to know what the percent RAS rate is relative to the influent flow. Calculate the RAS rate given the following information: MLSS concentration is 2500 mg/L, influent flow is 4.0 mgd, RAS concentration is 7,000 mg/L, WAS concentration is 7,200 mg/L, WAS pump rate is 60 gpm.
6. An activated sludge process has three aeration basins. Each basin is 100 feet long, 35 feet wide, and 12 feet deep. The MLSS concentration is 2800 mg/L. There are two clarifiers. Each clarifier is 55 feet in diameter and 12 feet deep. A clarifier core sample indicates that the solids concentration in the clarifier is equivalent to 500 mg/L. If the RAS/WAS concentration is 6000 mg/L, find the WAS pumping rate in gallons per day to maintain a sludge age of 15 days.
7. For the plant described in problem #6, assume an influent BOD concentration of 325 mg/L and an influent flow of 2.5 MGD. If the desired F:M ratio is 0.20, should wasting be increased or decreased?
8. Estimate the sludge pumping time in minutes per day for a primary sludge pump removing 100 gpm of sludge at 5% total solids from a primary tank receiving a flow of 5.0 MGD. The primary influent contains 250 mg/L of TSS and the primary effluent contains 70 mg/L of TSS.
9. Given the following information, find the solids loading rate to the secondary clarifier.
 - a. Influent flow = 2 MGD
 - b. MLSS = 2500 mg/L
 - c. RAS = 6000 mg/L
 - d. RAS flow is 70% of influent flow
 - e. Secondary clarifier is 65 feet in diameter and 12 feet deep.

1.A. Surface Overflow Rate = $\frac{\text{flow, gpd}}{\text{area, sf}}$

$$\frac{100 \text{ gal}}{\text{min}} \left| \frac{1440 \text{ min}}{1 \text{ day}} \right| = \frac{172800 \text{ gal}}{\text{d}}$$

$$\text{Area} = (0.785 \times \text{diameter})^2$$

$$\text{Area} = (0.785 \times 120 \text{ ft}) \times 120 \text{ ft}$$

$$\text{Area} = 11304 \text{ ft}^2$$

$$SOR = \frac{\text{flow}}{\text{area}}$$

$$SOR = \frac{172800 \text{ gal/d}}{11304 \text{ ft}^2}$$

$$SOR = 15.3 \text{ gal/d/sf}$$

B. Weir Loading Rate = $\frac{\text{Flow, gpd}}{\text{Linear feet of Weir}}$

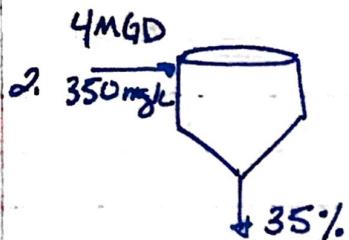
$$\text{Weir} = \text{Perimeter} = \pi d$$

$$\text{Perimeter} = (3.14)(120 \text{ ft})$$

$$\text{Perimeter} = 376.8 \text{ ft}$$

$$\text{Weir Loading Rate} = \frac{172,800 \text{ gpd}}{376.8 \text{ ft}}$$

$$\text{Weir Loading Rate} = 458.6 \text{ gpd/sf}$$



If it takes out 35%,
then 65% went on to
the secondary treatment process.

$$lbs/d = (m_8/L) \times MGD \times 8.34 \times 0.65$$

$$lb/d = (350 \text{ m}_8/\text{L}) \times 4 \text{ mgd} \times (8.34 \times 0.65)$$

$$lb/d = 7589.4$$

$$3.1. SVI, \text{m}_4/g = \frac{(SSV_{30}, \text{mL} \times 1000 \text{ m}_8/\text{g})}{MLSS, \text{m}_8/\text{L}}$$

$$SVI, \text{m}_4/g = \frac{(250 \text{ mL} \times 1000 \text{ m}_8/\text{g})}{3000 \text{ m}_8/\text{L}}$$

$$SVI, \text{m}_4/g = 83.3$$

$$SVI, \text{m}_4/g = \frac{(SSV_{30}, \text{mL} \times 1000 \text{ m}_8/\text{g})}{MLSS, \text{m}_8/\text{L}}$$

$$SVI, \text{m}_4/g = \frac{(980 \text{ mL} \times 1000 \text{ m}_8/\text{g})}{8,000 \text{ m}_8/\text{L}}$$

$$SVI, \text{m}_4/g = 122.5$$

$$4. MCRT = \frac{\text{lbs MLSS} + \text{lbs Clarifier}}{\text{lbs WAS} + \underbrace{\text{lbs Effluent}}_{\text{you can usually ignore lbs in effluent}}}$$

* Find lbs for each area.

$$\text{lbs A-Basin} = (\text{m8/L}) \times \text{MGD} \times 8.34$$

$$\downarrow \quad = (2500 \text{ m8/L}) \times 0.3 \text{ mgd} \times 8.34 \\ \downarrow \quad = 6255$$

$$\text{lbs Clarifier} = (\text{m8/L}) \times \text{MGD} \times 8.34$$

$$\downarrow \quad = (600 \text{ m8/L}) \times 0.06 \text{ MGD} \times 8.34 \\ \downarrow \quad = 300.24$$

for WAS, we first have to convert the flow rate to MGD.

$$\frac{10 \text{ gal}}{\text{min}} \times \frac{1440 \text{ min}}{1 \text{ day}} \times \frac{1 \text{ MG}}{1000000 \text{ gal}} = 0.0144 \text{ MGD}$$

$$\text{lbs WAS} = (\text{m8/L}) \times \text{MGD} \times 8.34$$

$$\downarrow \quad = (7,000 \text{ mg/L})(0.0144 \text{ MGD}) \times 8.34 \\ \downarrow \quad = 840.672$$

Now, we have all the pieces.

$$MCRT = \frac{\text{lbs MLSS} + \text{lbs Clarifier}}{\text{lbs WAS}}$$

$$MCRT = \frac{6255 + 300.24}{840.672} \quad \leftarrow \text{DO THIS TOP BIT FIRST. THERE IS AN INVERSE PROPORTION}$$

$$MCRT = \frac{6555.24 \text{ lbs}}{840.672 \text{ lbs/d}}$$

$$MCRT = 7.8 \text{ days}$$

5. Many people think that if you leave the solids in the clarifier, they will thicken and compact. This is only true to a limited extent. The settleometer doesn't keep compacting all day. Does it? Nope. RAS/WAS concentration is easily predicted.

$$X_{RAS} = \left(\frac{Q}{Q_{RAS}} + 1 \right) X_{MSS}$$

$$\frac{7000 \text{ m}^3/\text{L}}{2500} = \left(\frac{4 \text{ mgd}}{Q_{RAS}} + 1 \right) \frac{2500 \text{ m}^3/\text{L}}{2500}$$

① move this by dividing both sides by 2500

$$2.8 = \frac{4 \text{ MGd}}{Q_{RAS}} + 1 - 1$$

② move the 1 by subtracting it from both sides

$$1.8 = \frac{4 \text{ MGd}}{Q_{RAS}}$$

THESE
TWO NUMBERS
CAN TRADE
PLACES

$$Q_{RAS} = \frac{4 \text{ MGd}}{1.8}$$

$$Q_{RAS} = 2.22 \text{ MGd}$$

$$\text{or } \frac{2.22}{4} \times 100 = 56\%$$

of
influent
flow

6. THIS IS AS HARD AS THE MATH EVER GETS

$$MCRT = \frac{\text{lbs A-Basin}}{\text{given}} + \frac{\text{lbs clarifier}}{\text{find}}$$

$\xrightarrow{\text{lbs WAS}}$

$\xrightarrow{\text{unknown}}$

$$\text{lbs A-basin} = (\text{m8/L}) \times \text{MGD} \times 8.34$$

\downarrow need volume.

$$\begin{aligned}\text{Volume} &= (\text{Length} \times \text{Width} \times \text{Depth})(\# \text{ basins}) \\ &= (100 \text{ ft} \times 35 \text{ ft} \times 12 \text{ ft}) \times 3 \\ &= 126000 \text{ cf}\end{aligned}$$

BUT, I NEED MILLION GALLONS

$$\frac{126000 \text{ cf}}{1 \text{ cf}} \left| \begin{array}{c} 7.48 \text{ gallons} \\ \downarrow \end{array} \right| \frac{1 \text{ MG}}{1,000,000 \text{ gal}} = 0.942 \text{ mg}$$

$$\begin{aligned}\text{lbs A-basin} &= (\text{m8/L})(\text{MGD}) \times 8.34 \\ &= (2800 \text{ m8/L}) \times 0.942 \text{ mg} \times 8.34 \\ &= 21997.6 \text{ lbs}\end{aligned}$$

NOW, WE NEED TO DO THE SAME THING FOR THE CLARIFIERS.

$$\begin{aligned}\text{Volume} &= (0.785)(\text{diameter})^2(\# \text{ of clarifiers})(\text{depth}) \\ \text{Volume} &= (0.785) \times 55 \text{ ft} \times (55 \text{ ft}) \times 12 \text{ ft} \times 2 \\ \text{Volume} &= 56991 \text{ cf}\end{aligned}$$

$$\frac{56991 \text{ cf}}{1 \text{ cf}} \left| \begin{array}{c} 7.48 \text{ gallons} \\ \downarrow \end{array} \right| \frac{1 \text{ MG}}{1,000,000 \text{ gal}} = 0.426 \text{ mg}$$

$$\text{lbs CLARIFIER} = (\text{m8/L}) \times \text{mg} \times 8.34$$

$$\text{lbs CLARIFIER} = (500 \text{ m8/L}) \times 0.426 \text{ mg} \times 8.34$$

$$= 1776.42$$

NOW, WE ARE READY TO GO BACK TO THE MCRT FORMULA.

$$\text{MCRT} = \frac{\text{lbs A-basin} + \text{lbs Clarifier}}{\text{lbs WAS}}$$

$$15 \text{ days} = \frac{(21997.6 \text{ lbs} + 1776.42 \text{ lbs})}{\text{lbs WAS}}$$

THIS DIVIDING
LINE ACTS JUST
LIKE A PARENTHESIS

$$15 \text{ days} = \frac{23,774.02 \text{ lbs}}{\text{lbs WAS}}$$

change places

$$\text{lbs WAS} = \frac{23,774.02 \text{ lbs}}{15 \text{ days}}$$

$$\text{lbs WAS} = 1584.9$$

great! we found pounds,
BUT we need gallons

$$\text{lbs/d WAS} = (\text{m8/L}) \times \text{mgd} \times 8.34$$

$$1584.9 \text{ lbs/d} = (6000 \text{ m8/L}) \times \text{mgd} \times 8.34 \quad * \text{simplify!}$$

$$\underline{1584.9} = \underline{(50040 \times \text{mgd})}$$

$$\frac{50040}{50040} = \frac{50040}{50040}$$

$$0.03167 = \text{mgd}$$

to move this,
divide both
sides

*not quite there...

$$\frac{0.03167 \text{ mg}}{\text{d}} \Big| \frac{1000000 \text{ gal}}{1 \text{ mg}} \Big| = \boxed{31,673 \text{ gallons/day}}$$

THE ANSWER!

$$\text{7. } \frac{F}{m} = \frac{\text{lbs BOD}}{\text{lbs MLSS}}$$

* if % volatile is unknown,
use MLSS instead of MLVSS

$$\text{lbs BOD} = (\text{mg/L}) (\text{mgd}) (8.34)$$

$$\downarrow = (325 \text{ mg/L}) (2.5 \text{ mgd}) (8.34)$$

$$= 6776.25$$

$$\frac{F}{m} = \frac{\text{lbs BOD}}{\text{lbs MLSS}}$$

$$\frac{F}{m} = \frac{6776.25 \text{ lbs}}{21997.6 \text{ lbs}}$$

$$\frac{F}{m} = 0.31$$

figured this out in
problem #6

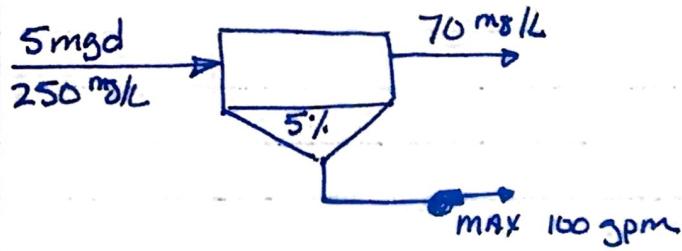
for this number to
get smaller, either BOD
must decrease or MLSS must increase.

to increase MLSS, decrease wasting



DECREASE

8. DRAW A PICTURE



SOLIDS CAN ONLY GO
TWO PLACES. FIND
TOTAL POUNDS GOING
TO THE BLANKET.

$$\text{lbs} = (\text{m}^3/\text{L}) \times \text{mgd} \times 8.34$$

$$\text{lbs} = (250 - 70 \text{ m}^3/\text{L}) \times 5 \text{ mgd} \times 8.34$$

$$\text{lbs} = 7506$$

BUT... THOSE SOLIDS GOT CONCENTRATED TO 5%.
IN THE BLANKET.

$1\% = 10,000 \text{ m}^3/\text{L}$ AS LONG AS WE ARE
UNDER ABOUT 7% SOLIDS

$$5\% \left| \frac{10,000 \text{ m}^3/\text{L}}{1\%} \right| = 50,000 \text{ m}^3/\text{L}$$

$$\text{lbs BLANKET} = (\text{m}^3/\text{L}) \times \text{MGD} \times 8.34$$

$$7506 \text{ lbs} = (50,000 \text{ m}^3/\text{L}) \times (\text{MGD}) \times 8.34 \quad \text{SIMPLIFY}$$

$$\frac{7506 \text{ lbs}}{417000} = \frac{(\text{417000} \times \text{MGD})}{417000}$$

$$0.018 = \text{MGD}$$

or

18,000 gallons per day.

~~SOLID PUMP DOES 100 gpm~~

$$\frac{18000 \text{ gallons}}{100 \text{ gal}} = \boxed{180 \text{ minutes total run time}}$$

DONE!

$$9. \text{ lbs/sf.d} = \frac{(Q_{INF} + Q_{RAS})(MLSS, m_8/L)(8.34)}{\text{AREA, SF}}$$

PIND THIS FIRST

$$\text{AREA} = (0.785 \times \text{diameter})^2$$

$$\text{AREA} = (0.785 \times 65 \text{ ft})^2 (65 \text{ ft})$$

$$\text{AREA} = 3316.625 \text{ ft}^2$$

RAS FLOW IS 70% OF INFLUENT FLOW

$$(2 \text{ mgd} \times 70\%) = 1.4 \text{ mgd}$$

$$\text{lbs/sf.d} = \frac{(Q_{INF} + Q_{RAS})(MLSS, m_8/L)(8.34)}{\text{AREA, SF}}$$

$$\text{lbs/sf.d} = \frac{(2 \text{ mgd} + 1.4 \text{ mgd}) \times 2500 \text{ m}_8/\text{L} \times 8.34}{3316.625 \text{ ft}^2}$$

$$\text{lbs/sf.d} = \frac{(3.4 \times 2500 \times 8.34)}{3316.625}$$

$$\text{lbs/sf.d} = 21.4$$